# Practical and Accurate Calculations of Radio Emission from EAS

Austin Cummings\*, Washington Carvalho Jr., Andrew Ludwig, Andres Romero-Wolf





#### How Do We Get Radio Emission?

$$\nabla \cdot \mathbf{E} = \frac{\rho}{\epsilon} \qquad \nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$
$$\nabla \cdot \mathbf{B} = 0 \qquad \nabla \times \mathbf{B} = \mu \mathbf{J} + \mu \epsilon \frac{\partial \mathbf{E}}{\partial t}$$

Step 2: Introduce scalar and vector potentials

$$\mathbf{B} = \nabla \times \mathbf{A}$$
$$\mathbf{E} = -\frac{\partial \mathbf{A}}{\partial t} - \nabla \phi$$

Step 3: Choose transverse gauge

 $\nabla \cdot \mathbf{A} = 0$ 

Step 4: Equations to solve

$$\nabla^2 \phi = -\frac{\rho}{\epsilon}$$
$$\nabla^2 \mathbf{A} - \mu \epsilon \frac{\partial^2 \mathbf{A}}{\partial^2 t} = -\mu \mathbf{J}_{\perp}$$

J. Alvarez-Muniz, A. Romero-Wolf, E. Zas, Phys.Rev.D81:123009

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$$\begin{split} \phi &= \frac{1}{4\pi\epsilon} \int \frac{\rho(\mathbf{x}',t')}{|\mathbf{x}-\mathbf{x}'|} d^3 \mathbf{x}' \\ \mathbf{A} &= \frac{\mu}{4\pi} \int \frac{\mathbf{J}_{\perp}(\mathbf{x}',t')}{|\mathbf{x}-\mathbf{x}'|} \delta\left(\sqrt{\mu\epsilon}|\mathbf{x}-\mathbf{x}'|-(t-t')\right) d^3 \mathbf{x}' dt' \end{split}$$

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Assume contributions from straight line travel

 $\mathbf{J}_{\perp}(\mathbf{x}',t') = e\mathbf{v}_{\perp}\delta^{3}\left(\mathbf{x}'-\mathbf{x_{0}}-\mathbf{v}t'\right)\left[\Theta(t'-t_{1})-\Theta(t'-t_{2})\right]$ 

Account for projection  $|\mathbf{x} - \mathbf{x_0} - \mathbf{v}t'| \simeq R - \mathbf{v} \cdot \hat{\mathbf{u}}t'$ 

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**Computationally expensive!** 

#### **Practical and Accurate Approach**

# **4-D Binning**

- Treat e<sup>±</sup> tracks within 4-D volumes as effective single tracks
- Reduces number of computations by a factor N, the number of tracks contained in an average volume
- Preliminary cell size based on Fraunhofer limit:

$$L < L_F = \frac{1}{\sin\theta} \sqrt{\frac{\lambda |\vec{R}|}{2\pi}}$$

- Essentially, a thinning oriented towards radio emission
  - Standard particle thinning is blind to radio calculations





## **OctTree Binning**

- Fraunhofer condition dependent on both frequency and distance to observer
   Less efficiency for precision at higher frequencies/closer observation
- Cells are bisected until they pass the Fraunhofer limit



• Let's define emission from the center of a track:

$$\circ t' = \frac{n_{\text{eff}}R}{c} + t$$

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#### **Example Performance**







- Basic methodology works well for low frequencies
  - $\circ~$  Peak E field within 10%
  - Beam pattern captured well (geomagnetic/Askaryan)
- Significant performance improvements
  - Average tracks/cell: ~20
  - Maximum tracks/cell: 200,000
- Lower accuracy at high frequencies
  - In particular for large viewing angles

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- To combat this, consider cuts in lateral distance



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Consider maximum and minimum observer times



• Assume the following shape parameterization:

$$VP(t) = \begin{cases} 0 & t \le t_{\min} \\ A(t - t_{\min})/(\bar{t} - t_{\min}) & t_{\min} \le t \le \bar{t} \\ Ae^{-(t - \bar{t})/\sigma_t} & \bar{t} \le t \end{cases}$$

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- Seems to model the vector potential shape well, capturing particularly well the rising edge
- Breaks down when the number of tracks decreases



## Summary

- The practical and accurate methodology calculates averaged vector potentials in 4-D cells by summing currents
  - Reproduces expected beam patterns
  - Peak E field within 10% for low frequencies
  - Expected performance gain factor >20
- High frequency behavior is largely not right
  - Can be fixed by decreasing cell size and increasing computational demand
- Profile shaping seems to be promising, but needs to be applied properly across the shower





#### Analytical n<sub>eff</sub> calculation

$$\mathcal{R}(h) = \mathcal{R}_s \exp(-K_r h) \quad \mathcal{R}_{eff} = \frac{1}{R} \int_0^R \mathcal{R}(h)$$
$$u^2 = s^2 + R_e^2 + 2sR_e \cos\theta_z$$
$$h(s) \approx s \cos\theta_z + \frac{s^2 \sin^2\theta_z}{2R_e} + \mathcal{O}(s^3)$$

$$\begin{aligned} \mathcal{R}_{eff} &= \frac{\mathcal{R}_s}{R} \frac{\sqrt{\pi R_e}}{\sqrt{2K_r} \sin \theta_z} \exp\left(\frac{K_r R_e \cos^2 \theta_z}{2 \sin^2 \theta_z}\right) \\ &\quad \text{erf}\left(\frac{\sqrt{K_r R_e}}{2 \sin \theta_z} \left(\cos \theta_z + \frac{s \sin^2 \theta_z}{R_e}\right)\right) \Big|_0^R \end{aligned}$$



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$$\frac{z}{z} = -R + \sqrt{L^{2} + R^{2} + 2RL(cos\theta)} = 1 + \frac{x}{2} - \frac{x^{2}}{8} + \cdots$$

$$= -R + R \sqrt{1 + \frac{L^{2}}{R^{2}} + \frac{2L}{R}(cos\theta)} = 1 + \frac{x}{2} - \frac{x^{2}}{8} + \cdots$$

$$= -R + R \left[ 1 + \frac{L^{2}}{2R^{2}} + \frac{L}{R}(cos\theta) - \frac{1}{8} \left[ \frac{L^{n}}{R^{2}} + \frac{4}{R^{2}} \frac{L^{2}}{6} + \frac{2}{R^{2}} \frac{L^{2}}{R^{2}} + \frac{2}{R^{2}} \frac{L^{2}}{R^{2}} \frac{L^{2}}{R^{2}} \frac{L^{2}}{R^{2}} + \frac{L^{2}}{2R} \frac{L^{2}}{R^{2}} \frac{L^{2}}{R^{2}}$$

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$$\mathcal{R}(h) = \mathcal{R}_s \exp(-K_r h) \quad \mathcal{R}_{eff} = \frac{1}{R} \int_0^R \mathcal{R}(h) \, dl$$
$$u^2 = s^2 + R_e^2 + 2sR_e \cos\theta_z$$
$$h(s) \approx s\cos\theta_z + \frac{s^2 \sin^2\theta_z}{2R_e} + \mathcal{O}\left(s^3\right)$$

$$\mathcal{R}_{eff} = \frac{\mathcal{R}_s}{R} \frac{\sqrt{\pi R_e}}{\sqrt{2K_r} \sin\theta_z} \exp\left(\frac{K_r R_e \cos^2\theta_z}{2\sin^2\theta_z}\right)$$
$$\operatorname{erf}\left(\frac{\sqrt{K_r R_e}}{2\sin\theta_z} \left(\cos\theta_z + \frac{\sin^2\theta_z}{R_e}\right)\right)\Big|_0^R$$



